TEST REPORT

SQM_653_2023

CUSTOMER

Kebe S.A.

PRODUCT NAME

NK250PLUS

TYPE OF PRODUCT

Masonry unit

TYPE OF TEST

Determination of the thermal design conductivity of the block and of masonry made with it

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Ordering Kebe S.A.
Product placed on the market from Kebe S.A. - 61100 Nea Santa - Kilkis - GREECE
Data related to the sample examined Masonry unit
Sample origin sampled and provided from the Customer
Manufacturing plant Kebe S.A. - 61100 Nea Santa - Kilkis - GREECE

Estimate prot. 23436/lab of 09/01/2023
Order confirmation email of 09/01/2023
Receipt of the samples -
Test execution September 2023
Laboratory and location of test execution Certimac - via Ravegnana, 186 - Faenza (RA)

Report issued 09/22/2023
Revision n° 00

Test executed by: Eng. Mattia Morganti
Report drafted by: Eng. Mattia Morganti
Approval: Technical director Eng. L. Laghi

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Chief Technical Officer
(Eng. Luca Laghi)

1. Object of the test

The following test report describes the determination of thermal design values of a masonry brick. The calculations were performed by means of a Finite Element Model implemented in Ansys 18.2 (Ref. 2-b), applied to a planar cross section (unit length), perpendicular to the holes axis and parallel to the thermal flux. In this calculation, the input data have been modified taking into account the effect of humidity as indicated by the technical standard in Ref. 2-a.

2. Reference standards and documents

The tests have been executed according to the methods defined in the following documentations and reference standards:

a. EN ISO 10456:2007. Building materials and products - Hygrothermal properties -Tabulated design values and procedures for determining declared and design thermal values (ISO 10456:2007)
b. CertiMaC calibration report 040219-C-17/Rev01. Calibration of a two-dimensional model for the calculation of the equivalent thermal conductivity of a masonry unit.
c. EN 6946:2008. Building components and building elements – Thermal resistance and thermal transmittance – Calculation method.
d. Test report SQM_652_2023, 09/22/2023 - Determination of the equivalent thermal conductivity of the block NK250PLUS and of masonry made with it.

3. Input data

The technical drawing of the block and the thermal conductivity of fired clay were supplied by the client (Figure 1). All input data used for the calculation are shown in Tables 1 and 2.

Figure 1. Geometry of the block

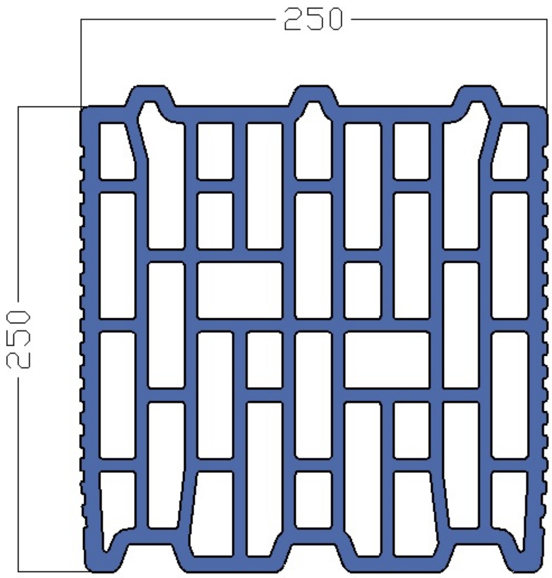

Table 1. Input data

Physical quantity	Nominal value	Ref.
Material thermal conductivity $\lambda_{10,dry,mat}$	0.401 W/mK	Provided by the Customer
Equivalent thermal conductivity of voids	Test Report NK250PLUS	Ref. 2-d

Table 2. Input data of the masonry

Masonry n. 1	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer
External plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer

Masonry n. 2	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer
External plaster	Thickness = 25 mm λ_{mortar} = 0.08 W/mK	Provided by the Customer

Masonry n. 3	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Not present	Provided by the Customer
External plaster	Not present	Provided by the Customer

4. Determination of the thermal design values

Thermal design values of the masonry are determined as defined by the standards at Ref. 2-a and 2-c, increasing the thermal conductivity of the materials in relation to the moisture content, using the following conversion coefficient (moisture content volume by volume):

$$F_m = e^{f_\psi(\psi_2-\psi_1)}$$

The standard sets as operating conditions a temperature of 23 °C and a relative humidity of 80% (precautionary hypothesis), which is related to the test condition at 10 °C, dry.

4. Results

Table 3 shows the results of the Finite Elements Analysis performed with design thermal values at Ref. 2-a.

Table 3. FEM results

Heat flow [W/m]	**Thermal coupling coefficient** L^{2D} [W/mK]	**Thermal transmittance** **U** [W/m²K]	**Total thermal resistance** R_T [m²K/W]	**True thermal resistance of the masonry unit** R_t [m²K/W]	**Equivalent thermal conductivity** $\lambda_{10,dry,unit}$ [W/mK]
1.7305	0.0865	0.3461	2.8893	2.7193	0.0919

5. Determination of thermal values of the masonry

Table 4 shows the thermal values of the masonry, in the three configurations described above, taking into account the effect of humidity.

Table 4. Results of the calculation for the masonry

Masonry n. 1	**Result**
Thermal resistance only of the layer R_t [m²K/W]	2.4860
Equivalent thermal conductivity of the masonry λ_{equ} [W/mK]	0.1207
Thermal resistance of the masonry including superficial thermal resistances R_T (m²K/W)	2.6560
Thermal transmittance **U** (W/m²K)	0.3765

Masonry n. 2	Result
Thermal resistance only of the layer R_t [m²K/W]	2.7122
Equivalent thermal conductivity of the masonry λ_{equ} [W/mK]	0.1106
Thermal resistance of the masonry including superficial thermal resistances R_T (m²K/W)	2.8822
Thermal transmittance **U** (W/m²K)	0.3470

Masonry n. 3	Result
Thermal resistance only of the layer R_t [m²K/W]	2.3934
Equivalent thermal conductivity of the masonry λ_{equ} [W/mK]	0.1045
Thermal resistance of the masonry including superficial thermal resistances R_T (m²K/W)	2.5634
Thermal transmittance **U** (W/m²K)	0.3901

SUMMARY TABLE OF RESULTS

The tests previously described gave the following results, taking into account the effect of humidity:

Product	Thermal design conductivity λ_{equ} [W/mK]	Thermal design transmittance U [W/m²K]
block NK250PLUS	**0.0919**	**0.3461**
Masonry n. 1	**0.1207**	**0.3765**
Masonry n. 2	**0.1106**	**0.3470**
Masonry n. 3	**0.1045**	**0.3901**

6. List of distribution

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In charged of technical test execution	**In charged of technical report drafting**	**Technical director Approval**
Eng. Mattia Morganti	Eng. Mattia Morganti	Ing. Luca Laghi

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-------- End of the Test Report ------

TEST REPORT

SQM_652_2023

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Chief Technical Officer
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1. Object of the test

The following test report describes the determination of the equivalent thermal values of a masonry brick. The calculations were performed by means of a Finite Element Model implemented in Ansys 18.2 (Ref. 2-b), applied to a planar cross section (unit length), perpendicular to the holes axis and parallel to the thermal flux.

2. Reference standards and documents

The tests have been executed according to the methods defined in the following documentations and reference standards:

a. EN 1745:2012. Masonry and masonry products – Methods for determining thermal properties.
b. CertiMaC calibration report 040219-C-17/Rev01. Calibration of a two-dimensional model for the calculation of the equivalent thermal conductivity of a masonry unit.
c. EN 6946:2008. Building components and building elements – Thermal resistance and thermal transmittance – Calculation method.

3. Input data

The technical drawing of the block and the thermal conductivity of fired clay were supplied by the client (Figure 1). All input data used for the calculation are shown in Table 1.

Figure 1. Geometry of the block

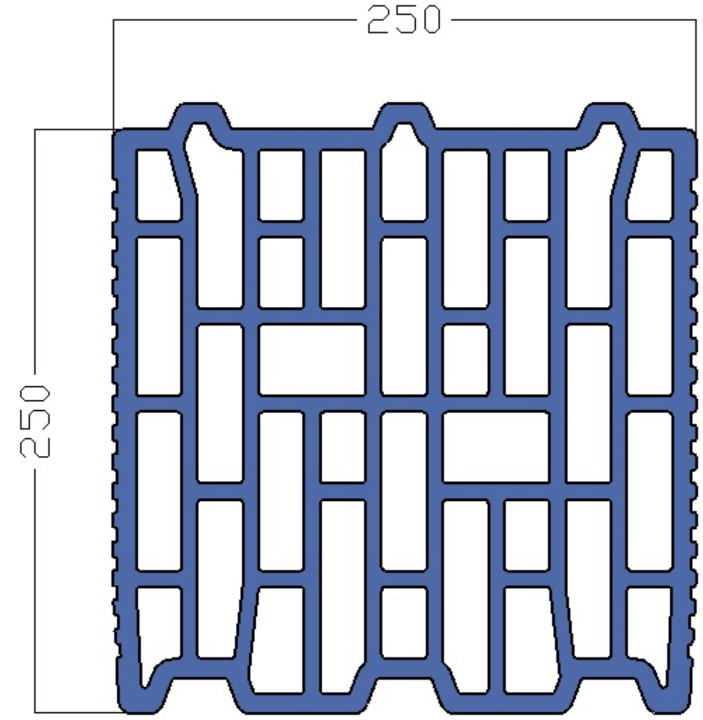
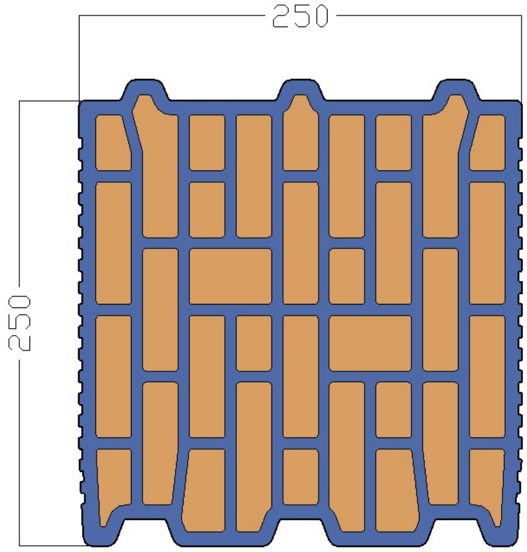


Table 1. Input data

Physical quantity	Nominal value	Ref.
Internal temperature Ti	20 °C = 293.15 K	Ref. 2-a and 2-c
External temperature Te	0 °C = 273.15 K	Ref. 2-a and 2-c
Internal superficial resistance Rsi	0.13 m^2K/W	Ref. 2-a and 2-c
External superficial resistance Rse	0.04 m^2K/W	Ref. 2-a and 2-c
Material thermal conductivity $\lambda_{10,dry,mat}$	0.401 W/mK	Provided by the Customer

All cavities are filled with NEOCOAT EPS 100 PLUS, whose conductivity is declared in the technical data sheet equal to 0.030 W/mK (Figure 2).

Figure 2. Cross section of the block



4. Results

Table 2 shows the results of the Finite Elements Analysis; Figures 3 and 4 graphically show the distribution of the isotherms and the vector state of the heat flow.

Table 2. FEM results

Heat flow [W/m]	**Thermal coupling coefficient** L^{2D} [W/mK]	**Thermal transmittance** U [W/m^2K]	**Total thermal resistance** R_T [m^2K/W]	**True thermal resistance of the masonry unit** R_t [m^2K/W]	**Equivalent thermal conductivity** $\lambda_{10,dry,unit}$ [W/mK]
1.6185	0.0809	0.3237	3.0893	2.9193	0.0856

Figure 3. Distribution of isotherms in the block [°C]

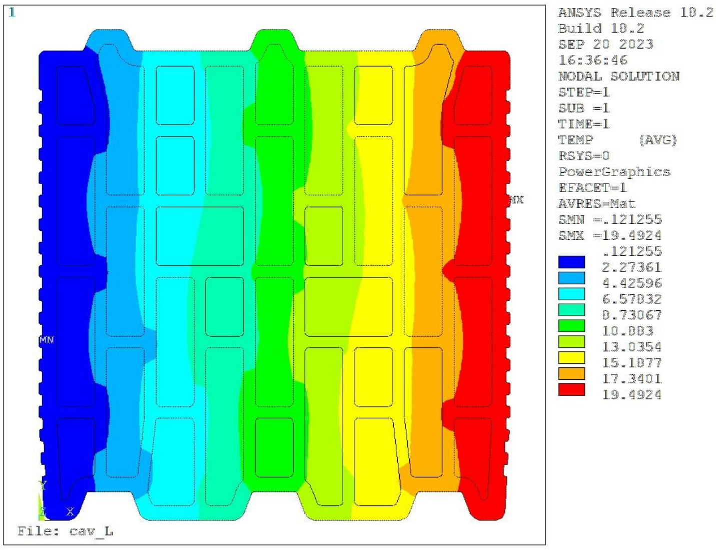
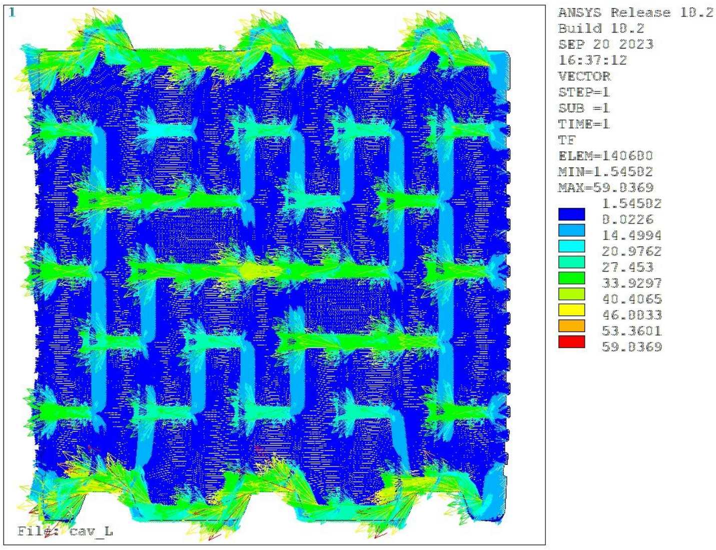


Figure 4. Average heat flow vectors [W/m^2]



5. Determination of thermal values of the masonry

Because of the interlocking block geometry, only horizontal mortar joints were considered. For the evaluation of the thermal values of the masonry, three different configurations were studied. The input data for the definition of the configurations are indicated in table 3.

Table 3. Input data of the masonry

Masonry n. 1	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer
External plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer

Masonry n. 2	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Thickness = 25 mm λ_{mortar} = 1.0 W/mK	Provided by the Customer
External plaster	Thickness = 25 mm λ_{mortar} = 0.08 W/mK	Provided by the Customer

Masonry n. 3	Nominal value	Ref.
Horizontal mortar joints	Thickness = 3 mm λ_{mortar} = 0.87 W/mK	Provided by the Customer
Internal plaster	Not present	Provided by the Customer
External plaster	Not present	Provided by the Customer

Tables 4, 5 and 6 show the thermal values of the masonry, in the three configurations described above.

Table 4. Results of the calculation for the masonry no. 1

Physical quantity	**Result**
Thermal resistance only of the layer $\mathbf{R_t}$ [m^{2}K/W]	2.7229
Equivalent thermal conductivity of the masonry $\boldsymbol{\lambda_{equ}}$ [W/mK]	0.1102
Thermal resistance of the masonry including superficial thermal resistances $\mathbf{R_T}$ (m^{2}K/W)	2.8929
Thermal transmittance **U** (W/m^{2}K)	0.3457

Table 5. Results of the calculation for the masonry no. 2

Physical quantity	**Result**
Thermal resistance only of the layer $\mathbf{R_t}$ [m^{2}K/W]	3.0104
Equivalent thermal conductivity of the masonry $\boldsymbol{\lambda_{equ}}$ [W/mK]	0.0997
Thermal resistance of the masonry including superficial thermal resistances $\mathbf{R_T}$ (m^{2}K/W)	3.1804
Thermal transmittance **U** (W/m^{2}K)	0.3144

Table 6. Results of the calculation for the masonry no. 3

Physical quantity	**Result**
Thermal resistance only of the layer $\mathbf{R_t}$ [m^{2}K/W]	2.6227
Equivalent thermal conductivity of the masonry $\boldsymbol{\lambda_{equ}}$ [W/mK]	0.0953
Thermal resistance of the masonry including superficial thermal resistances $\mathbf{R_T}$ [m^{2}K/W]	2.7927
Thermal transmittance **U** [W/m^{2}K]	0.3581

SUMMARY TABLE OF RESULTS

The tests previously described gave the following results:

Product	Equivalent thermal conductivity λ_{equ} [W/mK]	Thermal transmittance U [W/m²K]
block NK250PLUS	0.0856	0.3237
Masonry no. 1	0.1102	0.3457
Masonry no. 2	0.0997	0.3144
Masonry no. 3	0.0953	0.3581

6. List of distribution

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